

Qualifying Exam 2019
Select three problems

Dynamics

• **Problem 1: (10 points)**

Particles 1 and 2, each of mass m , are connected by a rigid massless rod of length l , as shown in Figure 1. Particle 1 can slide without friction along the floor while particle 2 can slide without friction on the wall. The dumbbell starts from rest with a lean angle $\theta=5^\circ$ and falls under the influence of gravity.

- 1- For what value of the angle θ will the dumbbell lose contact with the wall? (2 points)
(Hint: start with two generalized coordinates, x and θ , where x is the distance from the wall to particle 2, but impose constraint $x = 0$)
 - 2- For all that follows, consider the situation after the dumbbell loses contact with the wall (i.e., $x > 0$). Find the 2nd-order equations of motion for x and θ . (3 points)
- (c) Use the Routhian procedure to find a 2nd-order equation of motion for just the angle θ . (2 points)
- (d) Using constants of motion and initial conditions, find a 1st-order equation of motion of the form: (3 points)

$$\dot{\theta} = f(\theta)$$

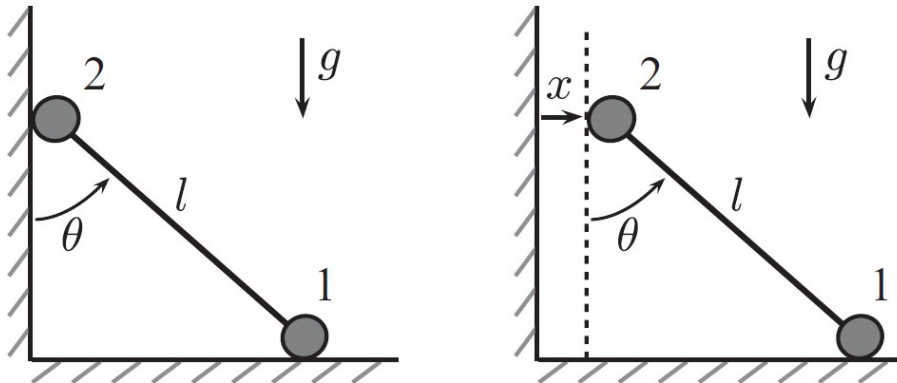


Figure 1

• **Problem 2: (10 points)**

Two masses, m_1 and m_2 , are connected by an inextensible string: m_1 moves on the horizontal table, while m_2 hangs suspended by the string below the table. The string passes through a hole in the center of the table, as shown in Figure 2. You may assume that m_2 moves only in the vertical direction, and that neither m_1 nor m_2 pass through the hole.

- 1- Determine the expression of the total energy of this dynamical system (2 points)
- 2- Assume $\dot{r}(t=0) = 0$ and apply the conservation of energy, determine a single scalar expression relating \dot{r} , $\dot{\theta}$, and r of the form: (3 points)

$$\dot{r}^2 = f(r, \dot{\theta})$$

where r is the distance from the hole to m_1 . It should be mentioned that there will be constants in the function f related to physical constants and initial conditions.

- 3- Use the angular momentum to reduce the previous single scalar expression from $\dot{r}^2 = f(r, \dot{\theta})$ to $\dot{r}^2 = f(r)$ (3 points)
- 4- Using the conservation of energy method, demonstrate that this dynamical system is governed by the following equation of motion: (2 points)

$$2\ddot{r} - \frac{r_0^4 \dot{\theta}_0^2}{r^3} + g = 0$$

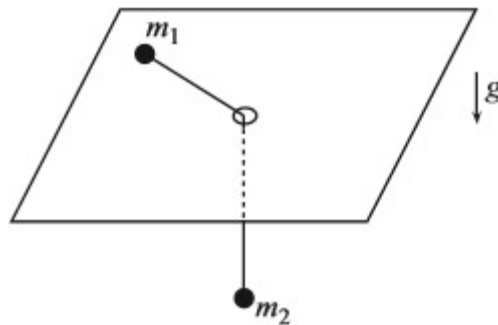


Figure 2

Vibrations

- **Problem 3: (10 points)**

The 2-DOF automobile model as shown in Figure 3 is considered. The mass of the automobile is M and the moment of inertia with respect of the center of mass is $J_o = Mr^2$.

- 1- Using Newton's second law and considering small oscillations, demonstrate that the general form of the equations of motion of the system can be expressed as: (2 points)

$$\begin{Bmatrix} \ddot{x} \\ \ddot{\theta} \end{Bmatrix} + \begin{bmatrix} \frac{2k_1 + k_2}{M} & \frac{k_2 l_2 - 2k_1 l_1}{M} \\ \frac{k_2 l_2 - 2k_1 l_1}{J_0} & \frac{k_2 l_2^2 + 2k_1 l_1^2}{J_0} \end{bmatrix} \begin{Bmatrix} x \\ \theta \end{Bmatrix} = \begin{Bmatrix} \frac{F(t)}{M} \\ \frac{T(t)}{J_0} \end{Bmatrix}$$

- 2- Why the stiffness matrix is not symmetric? (0.5 points)
- 3- Assume the parameters of this dynamical system are $M=350\text{Kg}$, $k_1=1000\text{N/m}$, $k_2=2400\text{N/m}$, $l_1=1\text{m}$, $l_2=2\text{m}$, and $r=1\text{m}$ (the radius of gyration about cg).
 - (a) Determine the natural frequencies and corresponding mode shapes and depict the mode shapes. (2 points)
 - (b) Check the orthogonality of modes and then determine the normal mode vibrations of the system when the initial conditions are $x(0) = 1$, $\theta(0) = -1$, and zero initial velocities. (1.5 points)
- 4- Consider the general form of the equations of motion as presented in question 1 and assume that $F(t)=2F_0 \cos(\Omega t)$ and $T(t)=T_0 \cos(\Omega t)$:
 - (a) Determine the moment of inertia J_o that renders the displacement of the car stationary (i.e., $\dot{x}(t) = 0$). (2 points)
 - (b) Determine the corresponding steady-state amplitude of the rotation. (2 points)

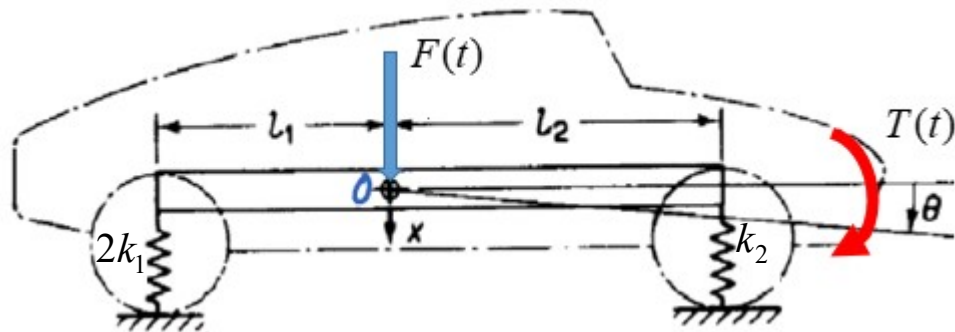


Figure 3

• **Problem 4: (10 points)**

- 1- Considering l as the free length of the spring with a stiffness k , demonstrate that the equations of motion of a spring-pendulum system shown in Figure 4 can be expressed as: (3 points)

$$m\dot{r} - m(l+r)\dot{\theta}^2 + kr - mg \cos(\theta) = 0$$

$$(l+r)\ddot{\theta} + 2\dot{r}\dot{\theta} + g \sin(\theta) = \frac{T(t)}{ml}$$

- 2- Determine the coupling terms and show their types (linear or nonlinear). Please justify. (1.5 points)
- 3- Assume small angles of oscillations, show that the linear form of the equations of motion can be expressed as: (1.5 points)

$$\begin{bmatrix} m & 0 \\ 0 & ml^2 \end{bmatrix} \begin{Bmatrix} \ddot{r} \\ \ddot{\theta} \end{Bmatrix} + \begin{bmatrix} k & 0 \\ 0 & mgl \end{bmatrix} \begin{Bmatrix} r \\ \theta \end{Bmatrix} = \begin{Bmatrix} mg \\ T(t) \end{Bmatrix}$$

- 4- Through a static analysis without any forcing, determine the equilibrium points (r_s, θ_s) of the system. (2 points)
- 5- Determine the natural frequencies of the system. (2 points)

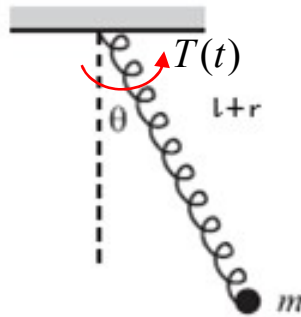


Figure 4

Formula Sheet

(QE 2019)

- Point P is fixed with the body

$$\frac{d\vec{op}^B}{dt} = 0, \text{ where: } \frac{d\vec{r}^N}{dt} = (\vec{\omega}_{(B/N)} \times \vec{r})$$

- P is moving w.r.t the body

$$\frac{d\vec{r}^N}{dt} = \frac{d\vec{op}^B}{dt} + (\vec{\omega}_{(B/N)} \times \vec{r})$$

- Translating & Rotating frame

$$\vec{R} + \vec{e} = \vec{r}$$

$$(\vec{V}^P)_N = (\vec{V}^B)_N + \frac{d\vec{p}^B}{dt} + (\vec{\omega}_{(B/N)} \times \vec{e})$$

- 5-part acceleration formula

$$(\vec{a}^P)_N = (\vec{a}^B)_N + \frac{d^N}{dt} \left(\frac{d\vec{e}^B}{dt} + (\vec{\omega}_{(B/N)} \times \vec{e}) \right)$$

$$(\vec{a}^P)_N = (\vec{a}^P)_B + (\vec{a}^B)_N + \left(2\vec{\omega}_{(B/N)} \times (\vec{V}^P)_B \right) + \left(\vec{\omega}_{(B/N)} \times (\vec{\omega}_{(B/N)} \times \vec{e}) \right) + \left(\alpha_{(B/N)} \times \vec{e} \right)$$

- Newton's 2nd Law

$$\sum \vec{F} = m\vec{a}$$

- Conservation of Energy

$$E = T + V ; E(t = t_1) = E(t = t_2)$$

$$\frac{d}{dt}(E) = 0$$

- Conservation of Angular Momentum

$$\vec{H}_O = m\vec{r} \times \dot{\vec{r}}$$

$$\dot{\vec{H}}_O = m\vec{r} \times \ddot{\vec{r}} = \vec{M}_O$$

$$\vec{H}_p = \sum_{i=1}^N \vec{\sigma}_i \times m\dot{\vec{\sigma}}_i$$

$$\dot{\vec{H}}_p = \vec{M}_p + \sum_{i=1}^N m_i \ddot{\vec{r}}_p \times \vec{\sigma}_i$$

- D'Alembert's Principle

$$\sum_{i=1}^N (\vec{f}_{ia} - m_i \ddot{\vec{r}}_i) \cdot \vec{B}_{ij} = 0 \quad \text{For } j=1,2,\dots,n$$

where $\vec{B}_{ij} = \frac{\partial \vec{r}_i}{\partial q_j}$

- Euler-Lagrange

$$L = T - V$$

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_i} \right) - \frac{\partial L}{\partial q_i} = Q_{nc-i}$$

Formula sheet - Final -

- Constrained version of Lagrange's equations:

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_i} \right) - \frac{\partial L}{\partial q_i} = Q_{nc-i} + C_i \rightarrow \text{constraint forces.}$$

$\underbrace{\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{q}_i} \right) - \frac{\partial L}{\partial q_i}}_{\text{Kinetic and conservative forces.}} + \underbrace{C_i}_{\text{Nonconservative forces.}}$

$$C_i = \sum_{j=1}^m \lambda_j a_{ji} \quad / \quad i = \{1, \dots, m\}$$

Where $a_{ji} = \frac{\partial \phi_j}{\partial q_i}$

- λ_j : Lagrange multipliers.
- m : number of constraints.
- n : number of generalized coordinates.
- $n - m$: number of degrees of freedom.

$$C_i = \sum_{k=1}^N \vec{f}_{k} \cdot \vec{\beta}_{ki} \quad / \quad i = \{1, \dots, m\}$$

$$Q_{nc-i} = \sum_{k=1}^N \vec{f}_{k} \cdot \vec{\beta}_{ki}$$

\vec{f}_{k} applied forces.

$$\vec{\beta}_{ki} = \frac{\partial \vec{r}_k}{\partial q_i} = \frac{\partial \vec{r}_k}{\partial q_i}$$

* Constraints

→ Holonomic: Constraints are function of position $\phi_j(q) = 0 \quad / \quad j = 1, \dots, m$

→ Non-holonomic: Constraints cannot be put into above form.

Most of them can be put in linear non-holonomic form:

$$\sum_{i=1}^n a_{ji}(q) \dot{q}_i = 0 \quad / \quad j = 1, \dots, m$$

number of constraints m

↳ find a_{ji} ?

Routh method:

↳ for handling "Ignorable coordinates".

$$\frac{\partial L}{\partial \phi} = 0 \Rightarrow \phi \text{ is an ignorable coordinate}$$

ϕ generalized coordinate

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\phi}} \right) - \frac{\partial L}{\partial \phi} = Q_{nc-\phi}$$

in case $Q_{nc-\phi} = 0$

$$\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{\phi}} \right) = 0 \Rightarrow \frac{\partial L}{\partial \dot{\phi}} = \text{const} = \beta_{\phi}$$

* Construct the Routhian function R :

$$R = L(\theta, \dot{\theta}, \dot{\phi}) - \beta_{\phi} \dot{\phi}$$

ϕ generalized coordinate

→ Routh equation:

$$\frac{d}{dt} \left(\frac{\partial R}{\partial \dot{\theta}} \right) - \frac{\partial R}{\partial \theta} = 0$$

↳ looks like Lagrange's equation with $L \rightarrow R$

Formula Sheet

- $\omega_n = \sqrt{\frac{k}{m}}$
- $\frac{c}{m} = 2\xi\omega_n$
- $f_n = \frac{\omega_n}{2\pi}$

1- Forced excitations

- EoM

$$\ddot{x} + 2\xi\omega_n\dot{x} + \omega_n^2x = F_0 \cos(\omega t)$$

- Particular solution (general form)

$$x_p = X_1 \cos(\omega t) + X_2 \sin(\omega t) = X \sin(\omega t + \phi)$$

where

$$X_1 = \frac{(\omega_n^2 - \omega^2)F_0}{(\omega_n^2 - \omega^2)^2 + (2\xi\omega_n\omega)^2} \text{ and } X_2 = \frac{(2\xi\omega_n\omega)F_0}{(\omega_n^2 - \omega^2)^2 + (2\xi\omega_n\omega)^2}$$

$$X = \sqrt{X_1^2 + X_2^2} \text{ and } \phi = \tan^{-1}\left(\frac{X_1}{X_2}\right)$$

- Amplitude of oscillations

$$\frac{X}{\Delta_{st}} = \left(\frac{1}{\sqrt{(1-r^2)^2 + (2\xi r)^2}} \right) \text{ where } r = \frac{\omega}{\omega_n} \text{ and } \Delta_{st} = \frac{F}{k} \text{ and } F_0 = \frac{F}{M}$$

- Resonant frequency and amplitude

$$r_{peak} = \sqrt{1 - 2\xi^2} \text{ and } \frac{X_r}{\Delta_{st}} = \frac{1}{2\xi\sqrt{1 - \xi^2}}$$

2 – Base excitations

- EoM

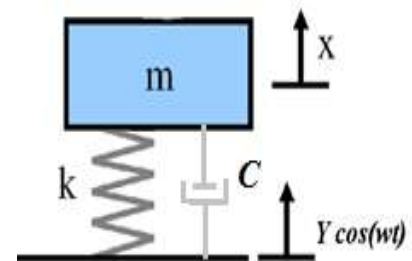
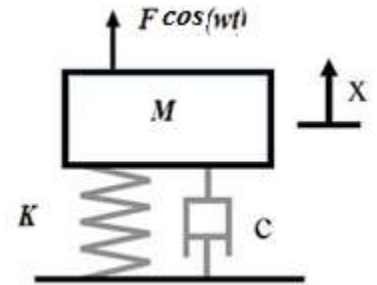
$$\ddot{x} + 2\xi\omega_n(\dot{x} - \dot{y}) + \omega_n^2(x - y) = 0$$

- $F_0 = Y\omega^2$
- Particular solution (general form)

$$z(t) = x(t) - y(t)$$

$$z(t) = Z_1 \cos(\omega t) + Z_2 \sin(\omega t) = Z \sin(\omega t + \Psi)$$

where



$$\frac{z_1}{Y} = \frac{(1-r^2)+(2\xi r)^2}{(1-r^2)^2+(2\xi r)^2} \text{ and } \frac{z_2}{Y} = \frac{2\xi r^3}{(1-r^2)^2+(2\xi r)^2}$$

- Amplitude of oscillations

$$X = \frac{\sqrt{1 + (2\xi r)^2}}{\sqrt{(1 - r^2)^2 + (2\xi r)^2}} Y$$

- Resonant frequency

$$r_{peak} = \frac{\sqrt{\sqrt{1+8\xi^2}-1}}{2\xi}$$

3 – Rotating unbalance

- EoM

$$\ddot{x} + 2\xi\omega_n\dot{x} + \omega_n^2x = \frac{m}{M}e\omega^2 \sin(\omega t)$$

- $F_0 = \frac{F}{M} = \frac{me\omega^2}{M}$
- Centrifugal force

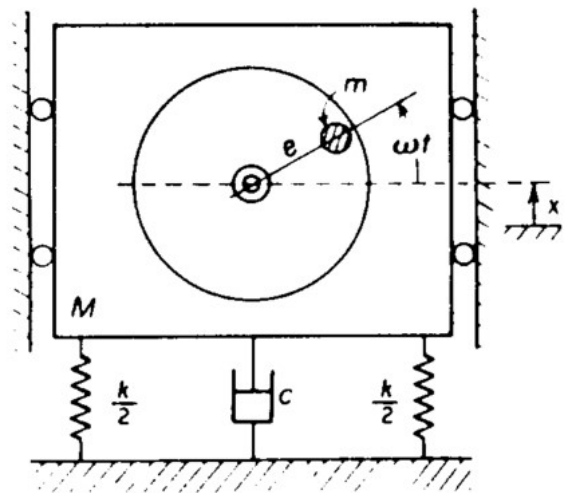
$$F_{centrifugal} = m \frac{v^2}{r}$$

- Amplitude of oscillations

$$X = \frac{me}{M} \frac{r^2}{\sqrt{(1 - r^2)^2 + (2\xi r)^2}}$$

- Resonant frequency and amplitude

$$r_p = \frac{\omega_r}{\omega_n} = \frac{1}{\sqrt{1-2\xi^2}} \text{ and } \frac{MX_r}{me} = \frac{1}{2\xi\sqrt{1-\xi^2}}$$



Formula sheet

1. Equations of Motion

$$[M]\{\ddot{x}\} + [K]\{x\} = \{F(t)\}$$

- Euler-Lagrange equations of a system having $q_1, q_2 \dots \dots q_n$ as degrees of freedom ($L=T-V$)

$$\frac{d\left(\frac{\partial L}{\partial \dot{q}_i}\right)}{dt} - \frac{\partial L}{\partial q_i} = Q_{nci}$$

- Law of Cosines

$$a^2 = b^2 + c^2 - 2bc * \cos(A)$$

2. Eigenvalue Problem (Free vibrations)

$$\{x(t)\} = \{X\}e^{j\omega t}$$

- Substitute EVP into EoM
- Solve for ω_1 and ω_2 (natural frequencies)
- Solve for X_1 and X_2 (always set $X_1 = 1$) to find Modal Vectors

3. Orthogonality/Orthogonal transformation (Free vibrations)

- Check for orthogonality

$$[\phi] = \{\text{Modal Vector}_{\omega=\omega_1}, \text{Modal Vector}_{\omega=\omega_2}\}$$

$$[\phi]^T[M][\phi] = \begin{bmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{bmatrix}$$

$$M_{11} = \{X\}_1^T [M]\{X\}_1$$

$$M_{12} = \{X\}_1^T [M]\{X\}_2 = 0$$

$$M_{21} = \{X\}_2^T [M]\{X\}_1 = 0$$

$$M_{22} = \{X\}_2^T [M]\{X\}_2$$

$$[\phi]^T[K][\phi] = \begin{bmatrix} K_{11} & K_{12} \\ K_{21} & K_{22} \end{bmatrix}$$

$$K_{11} = \{X\}_1^T [K]\{X\}_1$$

$$K_{12} = \{X\}_1^T [K]\{X\}_2 = 0$$

$$K_{21} = \{X\}_2^T [K]\{X\}_1 = 0$$

$$K_{22} = \{X\}_2^T [K]\{X\}_2$$

- *Orthogonal transformation:*

$$\{x(t)\} = [\Phi]\{y(t)\}$$

$$M_{11}\ddot{y}_1 + K_{11}y_1 = 0$$

$$M_{22}\ddot{y}_2 + K_{22}y_2 = 0$$

4. General Solution/Normal Mode Vibrations

$$\begin{pmatrix} x_1(t) \\ x_2(t) \end{pmatrix} = (A \cos \omega_1 t + B \sin \omega_1 t) \begin{pmatrix} X_1 \\ X_2 \end{pmatrix}_{\omega=\omega_1} + (C \cos \omega_2 t + D \sin \omega_2 t) \begin{pmatrix} X_1 \\ X_2 \end{pmatrix}_{\omega=\omega_2}$$

5. Absorber (forced vibrations)

$$[M] \begin{pmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{pmatrix} + [K] \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} = \begin{pmatrix} A \cos \Omega t \\ B \cos \Omega t \end{pmatrix}$$

- In complex form:

$$[M] \begin{pmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{pmatrix} + [K] \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} = \begin{pmatrix} A e^{j\Omega t} \\ B e^{j\Omega t} \end{pmatrix}$$

- Steady-state solutions (X_1, X_2)

$$\begin{pmatrix} x_1 \\ x_2 \end{pmatrix} = e^{j\Omega t} \begin{pmatrix} X_1 \\ X_2 \end{pmatrix}$$

- Inverse of a matrix

$$\begin{bmatrix} a & b \\ c & d \end{bmatrix}^{-1} = \frac{1}{ad - bc} \begin{bmatrix} d & -b \\ -c & a \end{bmatrix}$$