

Qualifying Exam, Fall 2021

Fluid Mechanics

- * This is a closed-book test (with a cheat sheet provided), and no calculator is allowed.
- * Work THREE out of the four problems, and clarify which three you want graded.

I want problems # _____, # _____, and # _____ to be graded.

Problem 1. The laminar boundary layer profile can be approximated by

$$u = \begin{cases} U \left[1 - \left(\frac{y}{\delta} - 1 \right)^2 \right] & y < \delta \\ U & \text{else} \end{cases}$$

Here, δ is the boundary layer thickness. The freestream velocity shall be constant: $U = \text{const.}$ and $\frac{\partial U}{\partial x} = 0$.

- a) Provide an expression for the displacement thickness, δ^* , as a function of δ .
- b) Provide an expression for the momentum thickness, ϑ , as a function of δ .
- c) Provide an expression for the skin-friction coefficient

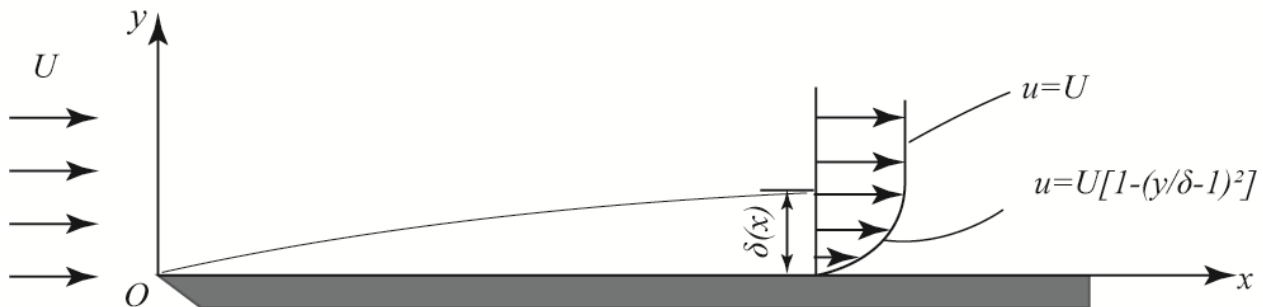
$$c_f = \frac{\tau_w}{\frac{1}{2} \rho U^2}$$

as a function of the boundary layer thickness Reynolds number, $Re_\delta = \frac{\rho U \delta}{\mu}$. The wall friction is $\tau_w = \mu \frac{\partial u}{\partial y}$.

The x-momentum equation can be integrated in y to obtain

$$\frac{1}{\rho} \tau_w = \frac{d}{dx} (U^2 \vartheta) + U \delta^* \frac{dU}{dx}$$

- d) From this equation, derive an expression for the skin-friction coefficient, c_f , as a function of δ .
- e) Set expressions for c_f from (c) and (d) equal to each other and find expression for Re_δ as a function of Re_x .
- f) Provide expressions for $\frac{\delta}{x}$ and c_f as a function of Re_x .

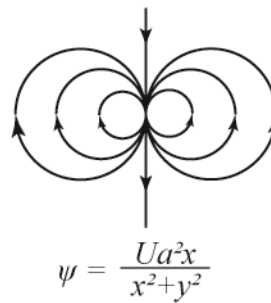
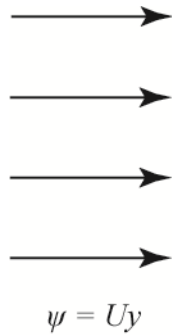


Problem 2. Consider a freestream in x that is superimposed with a dipole that is rotated by 90deg,

$$\Psi = U \left(y + \frac{a^2 x}{x^2 + y^2} \right)$$

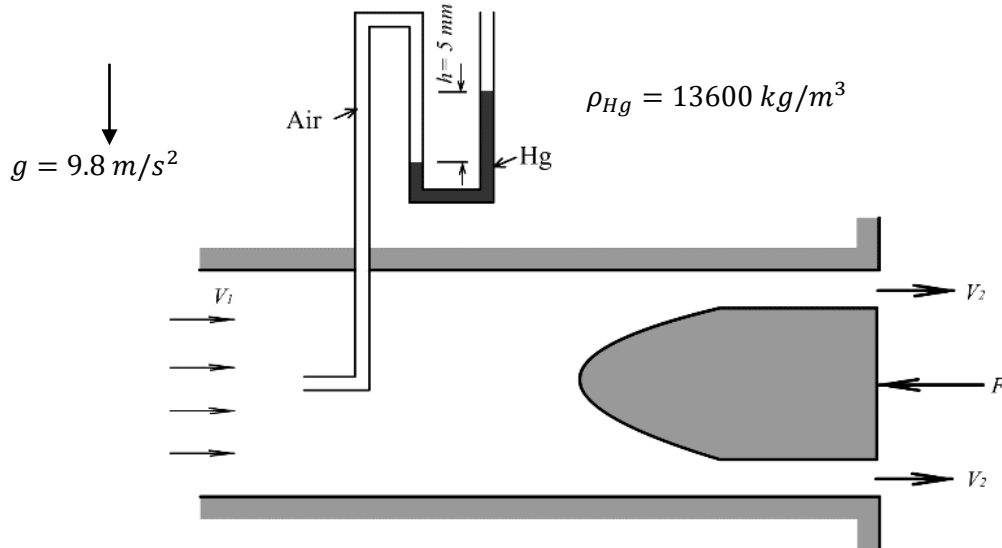
The freestream velocity shall be $U = 1$ and the dipole strength shall be $a^2 = 1$. Because of the dipole rotation, the resulting potential flow is NOT a model for the flow around a circular cylinder.

- Provide expressions for u and v as function of x and y .
- Provide expressions for $v_r = \frac{1}{r} \frac{\partial \Psi}{\partial \vartheta}$ and $v_\vartheta = -\frac{\partial \Psi}{\partial r}$ as function of r and ϑ .
- The flow has two stagnation points (saddle points). Provide r and ϑ locations for stagnation points.
- Provide analytical expression, $r = r(\vartheta)$, for streamlines passing through one of the stagnation points.
- Provide a rough sketch of the streamlines for the flow field (pencil and paper).



Problem 3. Air flows through a circular pipe with inside diameter of 0.5 m ($D_1 = 0.5\text{ m}$). A smoothly contoured plug of 0.4 m diameter ($D_2 = 0.4\text{ m}$) is held in the end of the pipe where air discharges to atmosphere (see figure below). Air density is $\rho = 1.3\text{ kg/m}^3$ and considered incompressible. Neglect the friction effects and assume uniform velocity profile at each cross-section. Determine:

- The mass flowrate through the pipe.
- Magnitude of force, F , required to hold the plug.

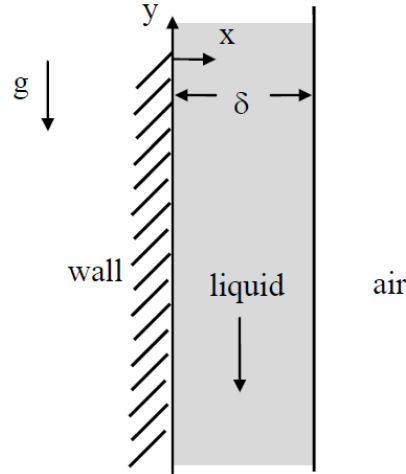


$$\text{COM: } \frac{\partial}{\partial t} \int_{CV} \rho dV + \int_{CS} \rho \vec{V} \cdot d\vec{A} = 0$$

$$\text{COLM: } \frac{\partial}{\partial t} \int_{CV} \rho \vec{V} dV + \int_{CS} \rho \vec{V} (\vec{V} \cdot d\vec{A}) = - \int_{CS} p d\vec{A} + \vec{F}$$

Problem 4. A viscous, incompressible, Newtonian liquid flows in steady, laminar, planar flow down a vertical wall. The thickness, δ , of the liquid film remains constant. Since the liquid free surface is exposed to atmospheric pressure, there is no pressure gradient in the liquid film. Furthermore, the air provides a negligible resistance to the motion of the fluid. Fluid density is ρ and dynamic viscosity is μ . Assume flow is fully developed ($\frac{\partial \vec{v}}{\partial y} = 0$).

- Determine the velocity distribution for this gravity driven flow. Clearly state all assumptions and boundary conditions.
- Determine the shear stress acting on the wall by the fluid.
- Determine the maximum velocity magnitude of the flow.



Continuity equation: $\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$

Navier-Stokes Equations:

$$\rho \left(\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} \right) = -\frac{\partial p}{\partial x} + \rho g_x + \mu \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right)$$

$$\rho \left(\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} \right) = -\frac{\partial p}{\partial y} + \rho g_y + \mu \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2} \right)$$

$$\rho \left(\frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} \right) = -\frac{\partial p}{\partial z} + \rho g_z + \mu \left(\frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} + \frac{\partial^2 w}{\partial z^2} \right)$$